

## **Physics Simulation**

- · Serve as an inductive bias for learning algorithms
- Utilize the power of deep learning to solve physics problems















## **Key Contributions**

- Dynamic collision detection to reduce collision dimensionality
- Gradient computation of collision response using implicit differentiation
- Optimized backpropagation using QR decomposition





## **Collision Response**

- Collision Detection:  $dist(node_i, face_j, t) < \delta$ , where  $\delta$  is the cloth thickness, and t is some time between two steps.
- Objective: introduce minimum energy to avoid collision:

$$dist(node_i, face_j, t) - \delta \ge 0$$

- Constraint formulation:  $\mathbf{Gx} + \mathbf{h} \leq 0$
- Objective formulation: Quadratic Programming:

$$\begin{array}{ll} \underset{\mathbf{z}}{\text{minimize}} & \frac{1}{2}(\mathbf{z} - \mathbf{x})^{\top} \mathbf{W}(\mathbf{z} - \mathbf{x}) \\ \text{subject to} & \mathbf{G}\mathbf{z} + \mathbf{h} \leq \mathbf{0} \end{array}$$

## Gradients of Collision Response

• Karush-Kuhn-Tucker (KKT) condition:

$$\mathbf{W}\mathbf{z}^* - \mathbf{W}\mathbf{x} + \mathbf{G}^\top \lambda^* = 0$$
$$D(\lambda^*)(\mathbf{G}\mathbf{z}^* + \mathbf{h}) = 0$$

• Implicit differentiation:

$$\begin{bmatrix} \mathbf{W} & \mathbf{G}^{\top} \\ D(\lambda^*)\mathbf{G} & D(\mathbf{G}\mathbf{z}^* + \mathbf{h}) \end{bmatrix} \begin{bmatrix} \mathbf{d}\mathbf{z} \\ \mathbf{d}\lambda \end{bmatrix} = \begin{bmatrix} \mathbf{M}\mathbf{d}\mathbf{x} - \mathbf{d}\mathbf{G}^{\top}\lambda^* \\ -D(\lambda^*)(\mathbf{d}\mathbf{G}\mathbf{z}^* + \mathbf{d}\mathbf{h}) \end{bmatrix}$$

49

## Gradients of Collision Response

• Solution:

$$\frac{\partial \mathcal{L}}{\partial \mathbf{x}} = \mathbf{d}_{\mathbf{z}}^{T} \mathbf{W}$$
$$\frac{\partial \mathcal{L}}{\partial \mathbf{G}} = -D(\lambda^{*}) \mathbf{d}_{\lambda} \mathbf{z}^{*\top} - \lambda^{*} \mathbf{d}_{\mathbf{z}}^{\top}$$
$$\frac{\partial \mathcal{L}}{\partial \mathbf{h}} = -\mathbf{d}_{\lambda}^{T} D(\lambda^{*}).$$

where  $d_z$  and  $d_\lambda$  is provided by the linear equation:

$$\begin{bmatrix} \mathbf{W} & \mathbf{G}^{\top} D(\lambda^*) \\ \mathbf{G} & D(\mathbf{G} \mathbf{z}^* + \mathbf{h}) \end{bmatrix} \begin{bmatrix} \mathbf{d}_{\mathbf{z}} \\ \mathbf{d}_{\lambda} \end{bmatrix} = \begin{bmatrix} \frac{\partial \mathcal{L}}{\partial \mathbf{z}}^{\top} \\ \mathbf{0} \end{bmatrix}$$

50



## Results

- Speed improvement in backpropagation.
- Scene setting: A large piece of cloth crumpled inside a pyramid.

Mesh	Baseline		Ours		Speedup	
Resolution	Matrix Size	Run Time (s)	Matrix Size	Run Time (s)	Matrix Size	Run Time
16x16	$599 \pm 76$	$0.33\pm0.13$	$66\pm26$	$\textbf{0.013} \pm \textbf{0.0019}$	8.9	25
32x32	$1326\pm23$	$1.2\pm0.10$	$97\pm24$	$\textbf{0.011} \pm \textbf{0.0023}$	13	112
64x64	$2024\pm274$	$4.6\pm0.33$	$242 \pm 47$	$\textbf{0.072} \pm \textbf{0.011}$	8.3	64

# The runtime performance of gradient computation is significantly improved by up to *two orders of magnitude*

## Results

- Application: Material estimation
- Scene setting: A piece of cloth hanging under gravity and a constant wind force.

Method	Runtime (sec/step/iter)	Density Error (%)	Non-Ln Streching Stiffness Error (%)	Ln Streching Stiffness Error (%)	Bending Stiffness Error (%)	Simulation Error (%)
Baseline	-	$68\pm46$	$74\pm23$	$160 \pm 119$	$70\pm42$	$12 \pm 3.0$
L-BFGS [30]	$2.89\pm0.02$	$4.2\pm5.6$	$64 \pm 34$	$72\pm90$	$70 \pm 43$	$4.9 \pm 3.3$
Ours	$\textbf{2.03} \pm \textbf{0.06}$	$\textbf{1.8} \pm \textbf{2.0}$	$57\pm29$	$45\pm41$	$77\pm36$	$\textbf{1.6} \pm \textbf{1.4}$

## Our method achieves the best runtime performance & the smallest error

53

### 53

## Results

- Application: Motion control
- Scene setting: A piece of cloth being lifted and dropped to a basket.

Method	Error (%)	Samples
Point Mass	111	_
PPO [18]	432	10,000
Ours	17	53
Ours+FC	39	108

# Our method achieves the best performance with a much smaller number of simulations





# Scalable Differentiable Physics for Learning and Control

Yi-Ling Qiao<sup>1</sup>, Junbang Liang<sup>1</sup>, Vladlen Koltun<sup>2</sup>, and Ming C. Lin<sup>1</sup>

<sup>1</sup>University of Maryland at College Park

<sup>2</sup>Intel Labs

https://gamma.umd.edu/researchdirections/mlphysics/diffsim/

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57



## **Motivation**

- Scalable Differentiable Physics
  - 0 Large number of interacting objects
  - Non-trivial shapes 0
  - Large variety of object sizes 0
  - Different physical properties/material types 0



59

## **Our Approach**

- 1. Scalable
  - Localized collision handling 0
  - Fast differentiation 0
- 2. General
  - Modeling different objects 0
  - 0
- collisions are sparse
- compute the gradients efficiently in large scenes
- mesh scales well and can model complex objects
- Interaction between different dynamics coupling between rigid body and cloth









Mesh Simulation Flow

- 1. Init  $\mathbf{x}_0, \mathbf{v}_0, \Delta t, t = 0$
- 2. Compute  $\Delta \mathbf{v}$  from  $\mathbf{x}_t, \mathbf{v}_t$  $\circ \Delta \mathbf{v} = \mathbf{M}^{-1} \mathbf{f}(\mathbf{x}_{t+1}, \mathbf{v}_{t+1}) * \Delta t$
- 3.  $\tilde{\mathbf{x}}_{t+1} = \mathbf{x}_t + \tilde{\mathbf{v}}_{t+1} * \Delta t, \tilde{\mathbf{v}}_{t+1} = \mathbf{v}_t + \Delta \mathbf{v}$
- 4.  $\mathbf{x}_{t+1}, \mathbf{v}_{t+1} = \text{resolve\_collision}(\mathbf{\tilde{x}}_{t+1}, \mathbf{\tilde{v}}_{t+1})$
- 5. t = t + 1, goto 2

67













## Our Goal

- Scalability regarding resolution and shape
  - Mesh-based representation
- Scalability regarding material and quantity
  - $\circ$   $\;$  Coupled physics between rigid body and deformable cloth
  - Localized collision handling

## **Key Contributions**

- Adopting meshes as a general representation of objects.
- Leveraging the structure of contacts by grouping using localized impact zones
- An acceleration scheme that can handle the nonlinear constraints using implicit differentiation
- Demonstration examples on applications to learning and control scenarios, where the presented framework outperforms derivative-free and model-free base-lines by at least an order of magnitude.



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- Global LCP solve for rigid bodies
  - Good at static contacts and static frictions
  - Difficult to couple with other materials
  - Slow
- Local constraint solver for clothes
  - Impulse-based solution: easy to couple between different materials
  - Solve within independent zones: faster computation
  - Unstable for large scale static contacts

## **Collision Handling**

- Global LCP solve for rigid bodies
  - Good at static contacts and static frictions
  - Difficult to couple with other materials
  - Slow
- Local constraint solver for clothes
  - o Impulse-based solution: easy to couple between different materials
  - Solve within independent zones: faster computation
  - Unstable for large scale static contacts

77

















## **Results - Scalable**

- Scale the number of objects
- Scene setting: A bunch of (20 1000) objects collide with the ground.
  - Methods: Ours vs. ChainQueen[8] (on CPU, for 2 second)
  - Scale the number of objects, while keeping the density of collisions and objects
  - When the number of object scales from 20 to 200, the grid size of ChainQueen[8] scales from 64 to 640



87

87

## **Results - Scalable**

- Scale the number of objects
- Scene setting: A bunch of (20 1000) objects collide with the ground.
- Our method scales well (linearly) in large scenes with big number of objects.





- Scale the resolution
- Scene setting: A bunny and a piece of cloth. Vary the relative sizes of cloth.
  - Methods: Ours vs. ChainQueen[8] (on CPU, for 2 second)
  - The relative size of two cloths: n:1.
  - $\circ$  n scales from 1 to 10.
  - The grid size of ChainQueen[8] scales from 64 to 640



















## **Results - General**

- Two-way coupling between cloth and rigid body
- Scene setting: Cloth & dominos

















- Derive the adjoint formulations for the entire articulated body simulation workflow, enabling a 10x acceleration over autodiff tools
- Adapt the checkpointing method to the structure of articulated body simulation to reduce memory consumption by 100x, making stable collection of extended experiences feasible
- Introduce two general schemes for accelerating reinforcement learning using differentiable physics
- Demonstrate the utility of differentiable simulation of articulated bodies in motion control and parameter estimation, enhancing performance in these scenarios by more than an order of magnitude



































## Motivation

• A Compliant Hand Based on a Novel Pneumatic Actuator.





## OBJECTIVE

- Differentiable Physics Simulator to support different scenarios
  - Complex Contact
  - Embedded Skeleton
  - Joint, muscle, and pneumatic actuators

124

# **Key Contributions**

- A *top-down matrix assembly* algorithm within <u>Projective Dynamics to</u> make soft-body dynamics compatible with reduced-coordinate articulated system
- An **extended and generalized dry friction model** for soft solids with a new matrix splitting strategy to stabilize the solver
- Analytical models of muscles, joint torques, and pneumatic actuators to enable more realistic and stable simulation results
- A **unified differentiable framework** that incorporates skeletons, contact, and actuators to enable gradient computation for learning and optimization
- Experimental validation demonstrating that differentiable physics accelerates system identification and motion control with soft articulated bodies up to orders of magnitude

124

# Background

Projective dynamics

Implicit Euler :
$$\mathbf{M}(\mathbf{q}_{n+1} - \mathbf{q}_n - h\mathbf{v}_n) = h^2(\nabla E(\mathbf{q}_{n+1}) + \mathbf{f}_{ext})$$
Solve: $\mathbf{q}_{n+1} = \operatorname*{arg\,min}_{\mathbf{q}} \frac{1}{2h^2}(\mathbf{q} - \mathbf{s}_n)^\top \mathbf{M}(\mathbf{q} - \mathbf{s}_n) + E(\mathbf{q})$ Local step: $E(\mathbf{q}) = \sum_i \frac{\omega_i}{2} \|\mathbf{G}_i \mathbf{q} - \mathbf{p}_i\|_F^2$ Global step: $\mathbf{q}_{n+1} = \operatorname*{arg\,min}_{\mathbf{q}} \frac{1}{2} \mathbf{q}^\top \left(\frac{\mathbf{M}}{h^2} + \mathbf{L}\right) \mathbf{q} + \mathbf{q}^\top \left(\frac{\mathbf{M}}{h^2} \mathbf{s}_n + \mathbf{J}\mathbf{p}\right)$ 

Method - rigid bodies:
$$\mathbf{q}_k = \mathbf{Q}\mathbf{T}_k^r\mathbf{V}_k$$
Metrices on rigid bodies: $\mathbf{q}_k^{i+1} = \mathbf{q}_k^i + \Delta \mathbf{q}_k^i = \mathbf{q}_k^i + \frac{\partial \mathbf{q}_k^i}{\partial \mathbf{z}_k} \Delta \mathbf{z}_k^i$ Linearize: $\mathbf{q}_k^{i+1} = \mathbf{q}_k^i + \Delta \mathbf{q}_k^i = \mathbf{q}_k^i + \frac{\partial \mathbf{q}_k^i}{\partial \mathbf{z}_k} \Delta \mathbf{z}_k^i$ Mew global step: $\Delta \mathbf{z}^i = \arg \frac{1}{\Delta \mathbf{z}} \Delta \mathbf{z}^T \mathbf{B}^T \left( \frac{\mathbf{M}}{h^2} + \mathbf{L} \right) \mathbf{B} \Delta \mathbf{z} + \Delta \mathbf{z}^T \mathbf{B}^T \left( \left( \frac{\mathbf{M}}{h^2} + \mathbf{L} \right) \mathbf{q}^i - \left( \frac{\mathbf{M}}{h^2} \mathbf{s}_k + \mathbf{J} \mathbf{p} \right) \right)$ Local step: $\mathbf{L}_k = \begin{bmatrix} \mathbf{L} + \omega_k^{i*} & \mathbf{q} \\ 0 & 0 \end{bmatrix} \mathbf{T}_k^r + \begin{bmatrix} \mathbf{0} & \mathbf{l}_k^i \\ 0 & 0 \end{bmatrix} = \mathbf{U} \mathbf{\Sigma} \mathbf{V}^T$ 

Method - Articulated body					
Skeleton tree:	$\mathbf{T}_k^r = \prod_u \mathbf{A}_u$	A is the local transformation matrix			
Jacobian: $\mathbf{B}_{u,v}$ =	$=\frac{\partial \mathbf{T}_{u}^{r}\mathbf{V}_{u}}{\partial \mathbf{z}_{v}}=\mathbf{Q}\mathbf{P}_{v}\frac{\partial \mathbf{A}_{v}}{\partial \mathbf{z}_{v}}\mathbf{S}_{v,u}\mathbf{V}$	$\mathbf{V}_{u}$			
Compute recursively:	$\mathbf{P}_v = \mathbf{P}_{v'} \mathbf{A}_{v'}$ $\mathbf{S}_{v',u} = \mathbf{A}_v \mathbf{S}_{v,u}$	P is the prefix product S is the suffix product			
		132			

### Method - Articulated body Algorithm 2 Matrix Assembly for the Articulated System 1: Input: tree link u2: Compute $\mathbf{P}_u$ using Eq. 16 3: $v \leftarrow u$ 4: while v is not root do Compute $S_{v,u}$ using Eq. 17 5: Compute $\mathbf{B}_{u,v}^{(u)}$ using Eq. 13 6: $v \leftarrow parent(v)$ 7: 8: end while 9: Compute $\mathbf{B}_{u,root}$ using Eq. 15 10: for s in descendants(u) do Solve link s recursively 11: 12: **end for**

## Method - Articulated body

**Rotational joint.** This joint is characterized by a rotation axis n and the angle  $\theta$ . Its transformation matrix and the Jacobian are:

$$\mathbf{A}^{r} = \begin{bmatrix} \mathbf{R} & \mathbf{0} \\ \mathbf{0} & 1 \end{bmatrix} \qquad \frac{\partial \mathbf{A}^{r}}{\partial \theta} = \begin{bmatrix} \frac{\partial \mathbf{R}}{\partial \theta} & \mathbf{0} \\ \mathbf{0} & 0 \end{bmatrix}$$
(18)

$$\mathbf{R} = \cos\theta \cdot \mathbf{I} + \sin\theta [\mathbf{n}]_{\times} + (1 - \cos\theta)\mathbf{n}\mathbf{n}^{\top}$$
(19)

$$\frac{\partial \mathbf{R}}{\partial \theta} = -\sin\theta \cdot \mathbf{I} + \cos\theta [\mathbf{n}]_{\times} + \sin\theta \mathbf{n} \mathbf{n}^{\top}$$
(20)

The local update of the rotational joint is given by:

$$\theta^{i+1} = \arctan(\sin\theta^i + \cos\theta^i \Delta\theta^i, \cos\theta^i - \sin\theta^i \Delta\theta^i)$$
(21)

134

134

## Method - Articulated body

**Prismatic joint.** This joint is characterized by a prismatic axis **u** and the scale *l*. Its transformation matrix and the Jacobian are:

$$\mathbf{A}^{p} = \begin{bmatrix} \mathbf{I} & l\mathbf{u} \\ \mathbf{0} & 1 \end{bmatrix} \qquad \frac{\partial \mathbf{A}^{p}}{\partial l} = \begin{bmatrix} \mathbf{0} & \mathbf{u} \\ \mathbf{0} & 0 \end{bmatrix}$$
(22)

(23)

135

The local update of the prismatic joint is simply addition:

$$l^{i+1} = l^i + \Delta l^i \tag{24}$$

$$\begin{split} & \Delta \mathbf{z}^{i} = \operatorname*{arg\,min}_{\Delta \mathbf{z}} \frac{1}{2} \Delta \mathbf{z}^{\top} \mathbf{B}^{\top} \begin{pmatrix} \mathbf{M} \\ h^{2} + \mathbf{L} \end{pmatrix} \mathbf{B} \Delta \mathbf{z} + \Delta \mathbf{z}^{\top} \mathbf{B}^{\top} \left( \begin{pmatrix} \mathbf{M} \\ h^{2} + \mathbf{L} \end{pmatrix} \mathbf{q}^{i} - \left( \frac{\mathbf{M}}{h^{2}} \mathbf{s}_{n} + \mathbf{J} \mathbf{p} \right) \right) (8) \\ & \text{Solve a linear system:} \qquad \begin{bmatrix} \mathbf{H}_{d} & \mathbf{H}_{c}^{\top} \\ \mathbf{H}_{c} & \mathbf{H}_{r}^{\top} \end{bmatrix} \begin{bmatrix} \Delta \mathbf{z}_{d}^{i} \\ \Delta \mathbf{z}_{r}^{i} \end{bmatrix} = \begin{bmatrix} \mathbf{k}_{d} \\ \mathbf{k}_{r} \end{bmatrix} \\ & \text{Torques can be added to K_r directly} \end{split}$$

## Method - Actuation - Pneumatic

**Pneumatic actuator.** We use co-rotational elastic strain energy model for tetrahedral cells. For a pneumatic cell with activation level *a*, the energy is computed as

$$\Psi_{pneumatic}(\mathbf{F}, a) = \frac{k_p}{2} \|\mathbf{F} - \mathbf{R}(a)\|^2$$
(27)

where the SVD decomposition of the deformation gradient is  $\mathbf{F} = \mathbf{U}\Sigma\mathbf{V}^T$ ,  $\mathbf{R}(a) = \mathbf{U}\Sigma^*\mathbf{V}^T$ ,  $\Sigma^* = \mathbf{D} + \Sigma$ , and  $\mathbf{D}$  is computed by

$$\arg\min_{\mathbf{D}} \left\| \mathbf{D} \right\|_{2}^{2}, s.t. \prod_{i} (\Sigma_{i} i + \mathbf{D}_{i}) = a$$
(28)

## Method - Actuation - Muscle

**Muscle actuator.** We use the muscle actuators described in [49]. Muscles are modeled as fibers in the soft bodies, and the forces are computed as  $\mathbf{f}_{muscle}(a) = -f_{muscle}(a)\mathbf{m}$ , where  $a \in [0, 1]$  is the activation level,  $\mathbf{m}$  is the direction of fiber. To achieve this force, a strain energy model [32] is used,  $E_{muscle} = \mathbf{V}_{muscle} \Psi_{muscle}(\mathbf{F}, e)$ , where  $\Psi_{muscle}(\mathbf{F}, a) = \frac{k_m}{2} ||(1 - r)\mathbf{Fm}||$ ,  $k_m$  is the stiffness,  $r = \frac{1-a}{l}$  is the projection of the cord segment,  $l = ||\mathbf{Fm}||$  is the stretch factor.

# Method - ContactOriginal global step: $\left(\frac{\mathbf{M}}{h^2} + \mathbf{L}\right) \mathbf{q}_{n+1} = \frac{\mathbf{M}}{h^2} \mathbf{s}_n + \mathbf{J} \mathbf{p}$ Convert to velocity space: $\mathbf{M} \mathbf{v}^{i+1} = \mathbf{f} - h^2 \mathbf{L} \mathbf{v}^i + \xi^i$ $\mathbf{f} = \mathbf{M} \mathbf{s}_n - (\mathbf{M} + h^2 \mathbf{L}) \mathbf{q}_n + h^2 \mathbf{J} \mathbf{p}$ Contact handling: $\xi^i$ Depends on the relative velocities/momentum of collided vertices



